

# Controlling cellular organization in bioprinting through designed 3D microcompartmentalization

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## ABSTRACT

Controlling cellular organization is crucial in the biofabrication of tissue-engineered scaffolds, as it affects cell behavior as well as the functionality of mature tissue. Thus far, incorporation of physiochemical cues with cell-size resolution in three-dimensional (3D) scaffolds has proven to be a challenging strategy to direct the desired cellular organization. In this work, a rapid, simple, and cost-effective approach is developed for continuous printing of multicompartamental hydrogel fibers with intrinsic 3D microfilaments to control cellular orientation. A static mixer integrated into a coaxial microfluidic device is utilized to print alginate/gelatin-methacryloyl (GelMA) hydrogel fibers with patterned internal microtopographies. In the engineered microstructure, GelMA compartments provide a cell-favorable environment, while alginate compartments offer morphological and mechanical cues that direct the cellular orientation. It is demonstrated that the organization of the microtopographies, and consequently the cellular alignment, can be tailored by controlling flow parameters in the printing process. Despite the large diameter of the fibers, the precisely tuned internal microtopographies induce excellent cell spreading and alignment, which facilitate rapid cell proliferation and differentiation toward mature biofabricated constructs. This strategy can advance the engineering of functional tissues.

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## I. INTRODUCTION

Cells in most tissues exhibit a high level of organization in their spatial distribution and alignment.<sup>1,2</sup> This organized architecture is critical to proper cellular development during maturation and the function of the mature tissue. Therefore, biofabricated cellular scaffolds for tissue engineering applications need to mimic this cellular architecture to reproduce the behaviors of natural tissue.<sup>3,4</sup> Various chemical or topological surface patterning approaches have been employed to provide cues for controlling the alignment of the cells, but these methods are limited to 2D culture and fail to translate into realistic *in vivo* conditions.<sup>5–7</sup> Researchers also have endeavored to fabricate 3D scaffolds with controlled spatial distribution and directed

alignment of the cells for various tissue engineering applications.<sup>8,9</sup> Cellular alignment in 3D scaffolds can be directed with similar chemical and topological patterning approaches to those currently used in 2D cell alignment. In some examples of such a technique, researchers used focused laser beams to pattern bioactive molecules inside 3D hydrogel scaffolds, which induced cellular elongation in a desired direction.<sup>10,11</sup> Furthermore, it has been demonstrated that confinement of cells in constructs with sufficiently small dimensions, fabricated through micromolding or photolithography, can direct elongation of the cells along the borders of the structure.<sup>12–14</sup> Modulation of cellular alignment is also shown to be possible through application of external stimuli, such as static and dynamic mechanical

stress<sup>15,16</sup> or electrical pulses.<sup>17,18</sup> While these methods have been shown to successfully fabricate miniaturized tissue models, they suffer from significant limitations, such as setup complexity, the negative impact of external fields on cells, limited construct size, multistep fabrication processes, and low throughput, presenting significant challenges for their clinical translation.

Re-creating a highly organized hierarchical structure is of particular importance when engineering anisotropic fibrillar tissues, such as muscles.<sup>19,20</sup> The directionality in these structures spans from their microscale cellular alignment to the macroscale, where densely packed fibers bundle together to form fascicles.<sup>21,22</sup> As a result, microengineered cellular structures need to be assembled using relevant strategies that enable this organization. Fiber-based biofabrication techniques have been implemented for engineering anisotropic tissues, such as muscles, due to the similarity of the formed fibrillar architectures and the native tissue.<sup>23,24</sup> Ranging from extrusion bioprinting<sup>25–27</sup> to biotextile processes,<sup>28</sup> fiber-based tissue engineering has been employed as a high-throughput, simple, and cost-effective method for assembly of cell-laden fibers. These fibers act as the building blocks of biomimetic fibrillar constructs for engineering muscle. Inherent directionality, enhanced mechanical properties, and control over geometry and composition of final structure are distinct advantages of fiber-based approaches in the context of muscle tissue engineering.<sup>23,24</sup> However, creating highly ordered cellular organization within the individual fibers of such constructs has proven challenging, since the dimensions of fibers compatible with biotextile processes and extrusion bioprinting are much larger than cell-scale sizes, reducing the boundary effects on cellular organization.<sup>20,29</sup> It has been demonstrated that the encapsulated cells' alignment decreases with increasing distance between the boundaries, with microfeatures larger than 100  $\mu\text{m}$  being unrecognizable to cells.<sup>12</sup>

A few approaches were successful in directing cellular organization in fiber-based scaffolds by incorporating intrinsic microstructures that provided guiding cues to the cells during their growth.<sup>30,31</sup> However, these methods require multistep fabrication processes, which makes them incompatible with bioprinting strategies. Here, we address this challenge by creating a compartmentalized fiber with internal hydrogel-based topographical cues to direct cellular growth and organization during tissue maturation. While controlling the fiber diameter in larger scales, the size of each compartment could also be easily tuned down to dimensions recognizable by cells to allow effective direction of cellular alignment within the fiber. To demonstrate the potential of the strategy, we investigated the effect of this biofabricated architecture on muscle cell growth, morphology, and function. This strategy can be easily applied to various fiber-based tissue engineering approaches, including 3D bioprinting and biotextile manufacturing, to control cellular organization, facilitating biofabrication of more biomimetic structures.

## 103 II. RESULTS

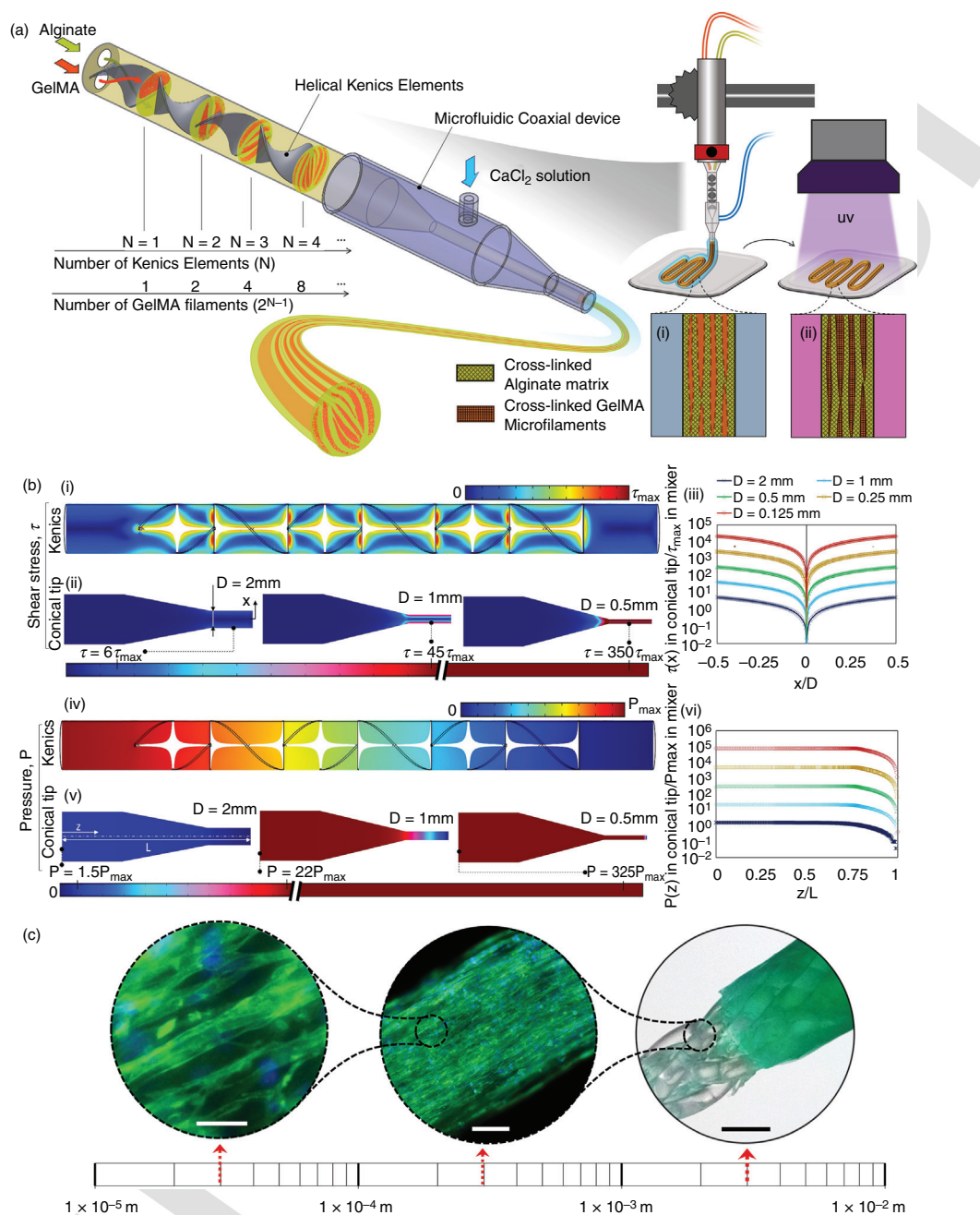
104 The process of fabricating multicompartmental hydrogel fibers  
105 (MCHFs) is depicted in Fig. 1. The proposed approach is based on the  
106 manipulation of different hydrogels' flow for construction of a com-  
107 partmentalized stream of the bioink. Alginate and GelMA were  
108 selected as hydrogels for this purpose. One of the main challenges in  
109 fiber-based biofabrication approaches, such as extrusion bioprinting  
110 and biotextile manufacturing, is the selection of a "cell-favorable"

bioink that can form a scaffold with high shape fidelity. This requires a relatively viscous precursor that can rapidly cross-link upon printing to form a robust and stable fiber.<sup>28,32</sup>

GelMA is a cell-permissive hydrogel that supports cell spreading and proliferation due to the presence of cell attachment sites, such as arginine-glycine-aspartic acid peptides, as well as matrix metalloproteinase-sensitive degradation motifs, suitable for cell remodeling.<sup>33,34</sup> However, due to its low viscosity and noninstantaneous photocrosslinking, direct formation of stable GelMA fibers is challenging.<sup>35</sup> A possible solution to overcome this is the incorporation of other hydrogels to enable GelMA fiber formation.<sup>35</sup> Alginate is a good candidate for mixing because it exhibits the necessary viscosity and rapid ionic gelation.<sup>36</sup> A hybrid GelMA/alginate bioink can easily be implemented in bioprinting<sup>37</sup> or biotextile strategies,<sup>29</sup> although the incorporation of alginate, which lacks cell attachment sites and biodegradable peptides, reduces the suitability of such bioinks for tissue engineering applications.<sup>38</sup>

In this study, we resolve this challenge through compartmentalization of the bioinks in such a way that distinct GelMA compartments support cell functionality while alginate compartments enable quick formation of stable fibers. A static mixer-integrated coaxial microfluidic device was employed for fabrication of MCHFs [Fig. 1(a) and Fig. S1]. A static mixer with an optimized number of mixing elements was implemented to divide the main streams of alginate and GelMA solutions into substreams with the desired thickness. This solution, with intercalated striations of GelMA and alginate, was then extruded through the inner channel of a coaxial microfluidic device and exposed to  $\text{Ca}^{2+}$  ions to stabilize the structure through gelation of the alginate. At this stage, the cross-linked alginate was physically confining the striations of GelMA precursor [Fig. 1(a), (i)]. UV irradiation was subsequently used to cross-link the GelMA within the alginate matrix and form internal microfilaments [Fig. 1(a), (ii)]. The final structure was a millimeter-scale hydrogel fiber with microscale internal topological features consisting of consecutive microfilaments of alginate and GelMA hydrogel. This multiscale fibrous structure can enable cells' spreading and alignment.

The subdivision of the different hydrogel streams into microscale substreams, embedded within the millimeter-scale flow, led to formation of internal features of a much smaller size than the diameter of the printed filament [Fig. 1(b)]. In conventional bioprinters, the minimum feature size is dictated by the nozzle diameter. As a result, improving the resolution comes at the cost of an increase in the shear stress applied to the encapsulated cells as well as an elevated pressure required for extrusion of viscous bioinks through the smaller nozzle.<sup>39</sup> However, in our printing strategy, resolutions are not shear dependent and are improved through the consecutive subdivision of streams without changing the nozzle diameter [Fig. 1(b), (i)]. Numerical simulation results demonstrated that while increasing the resolution using the static mixer does not significantly increase the shear stress inside the flow, a corresponding decrease in nozzle tip diameter to match the resolution enhanced with each additional static mixer element can increase the shear stress by approximately eightfold [Fig. 1(b), (ii) and (iii)]. Similarly, the extrusion pressure is not significantly increased by the static mixer due to its relatively large channel size ( $\sim 5$  mm; see Fig. S1), while the pressure increased by  $\sim 15$ -fold with decreasing the size of nozzle tip corresponding to the application of each additional static mixer element.



**FIG. 1.** Biofabrication of multicompartmental hydrogel fibers for formation of multiscale biomimetic constructs. (a) The fabrication setup consisted of a static mixer creating striations of different hydrogels integrated with a coaxial microfluidic device extruding the mixed streams of hydrogels through a sheath flow of  $\text{CaCl}_2$  to cross-link alginate and form the matrix of the fiber (i). The fibers were then exposed to UV light to cross-link the GelMA striations within the alginate matrix, creating an internal fibrous microstructure (ii).

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168 Alignment of cells within the hydrogel fiber, as will be discussed in  
 AQ2 169 Secs. II A–D, could establish a hierarchical multiscale construct, mim-  
 170 icking the structure of native fibrillar tissue [Fig. 1(c)]. The fabrication  
 171 method developed here is simple and cost effective, without any

requirement for special tools. In addition, its high throughput allows the 172  
 fabrication of cell-laden fibers at speeds up to meters per minute and 173  
 makes this method attractive for unconventional applications of tissue 174  
 engineering that requires mass production, such as lab-grown meat. 175



## 176 A. Characterization of multicompartamental hydrogel 177 fibers

178 The formation of MCHF with internal microfilaments is based  
179 on the controlled mixing of the two constituent precursors in the mix-  
180 ing nozzle (Fig. 2). A computational finite element simulation was  
181 implemented to elucidate the working principle of the static mixer-inte-  
182 grated coaxial microfluidic device. Figure 2(a) shows the computer-  
183 aided design (CAD) model of the static mixer used for the simulations.  
184 In this study, a Kenics-type static mixer,<sup>40,41</sup> which consists of multiple  
185 helical elements twisting intermittently in different directions, was  
186 used for formation of MCHF [Fig. 2(a)]. As indicated by simulations,  
187 each Kenics element in this setup divides the upstream of the flow into  
188 two substreams [Fig. 2(b)]. By injecting two different solutions into  
189 the mixer, the streams are consecutively divided into more substreams,  
190 forming an array of different striations. The total number of striations  
191 created using an N-element static mixer is therefore  $2^N$ , while the  
192 number of striations for each component will be  $2^{N-1}$ . Assuming a uni-  
193 form distribution, the thickness of each striation is then  $D_i/2^N$ , where  
194  $D_i$  is the final fiber diameter. Consequently, by controlling the number  
195 of elements in the static mixer, an internal structure with tunable  
196 thickness and number of striations can be formed. The cross section of  
197 flow clearly demonstrates the formed striations within the flow [Fig.  
198 2(c), top row].

199 The simulation results were validated experimentally. The Kenics  
200 element CAD design was 3D printed using a stereolithography 3D  
201 printer followed by its insertion into a barrel and integration with a  
202 coaxial microfluidic device [Fig. S1(a)]. The device was then used for  
203 evaluation of the flow profile generated by the static mixer. Immediate  
204 cross-linking of the structure through wet spinning of alginate into a  
205 calcium chloride ( $\text{CaCl}_2$ ) bath can preserve the internal microstructure  
206 of the fabricated fibers for analysis. Examining cross sections of experi-  
207 mentally generated fibers confirmed the formation of striations within  
208 the flow, which were cross-linked and formed the internal microfila-  
209 ments. Figure 2(c), bottom row, indicates the size dependency of the  
210 microfilaments to the number of the mixer elements.

211 Multicompartamental alginate/GelMA fibers were fabricated using  
212 the two-step cross-linking process just described. Figure 2(d) indicates  
213 the effect of mixing level on the internal microstructure of the fibers  
214 fabricated using this method. As expected, a fibrous structure can be  
215 generated in which increasing the number of Kenics elements  
216 decreases the size of internal microfilaments [Fig. 2(d), (i) and (ii)].  
217 Comparatively, a premixed bioink, prepared via vortex mixing and  
218 extruded through a static mixer-integrated microfluidic coaxial device,  
219 formed a homogeneous fiber without internal microfilaments [Fig.  
220 2(d), (iii)].

221 To demonstrate that the developed multicompartamental printing  
222 is not limited to the implemented materials (alginate and GelMA) or  
223 their specific cross-linking methods, we evaluated the compatibility of  
224 the strategy with two different materials, including Pluronic-F127 and  
225 Laponite nanoclay hydrogels. Our results demonstrated that the inter-  
226 nal microfilaments could be easily formed and preserved upon print-  
227 ing. Figure S2 illustrates the cross section and top view of the nanoclay  
228 MCHFs.

229 We further investigated the effect of the coaxial microfluidic  
230 device on the hydrogel fiber structure. The primary role of the coaxial  
231 microchannels is the induction of alginate gelation, making the fabri-  
232 cation strategy compatible with extrusion-based bioprinting. The

233 coaxial system further provides the opportunity of accurate control  
234 over the diameter of fabricated hydrogel fibers [Figs. 2(e) and 2(f)].  
235 Although the diameter of the fabricated fiber can also be adjusted by  
236 changing the size of the nozzle outlet, tuning the ratio of outer ( $\text{CaCl}_2$   
237 solution) channel flow rate  $Q_{\text{out}}$  to that of inner (multicompartamental  
238 hydrogel solution) channel  $Q_{\text{in}}$  offers real-time and accurate control  
239 over the size of final fiber. Simulation and experimental results demon-  
240 strated that by adjusting the  $Q_{\text{out}}/Q_{\text{in}}$  ratio, the orientation of internal  
241 microfilaments can be manipulated [Figs. 2(f) and 2(g)]. While a ratio  
242 of  $Q_{\text{out}}/Q_{\text{in}} \approx 1-2$  did not significantly change the orientation of  
243 formed internal microfilaments, a higher ratio could deform the  
244 streamlines, as shown by simulation results. Immediate gelation of  
245 alginate upon exposure to  $\text{Ca}^{2+}$  ions could preserve the formed micro-  
246 structure and even intensify it by solidifying the outer layers of the  
247 fiber while the fluid is still flowing in the inner layers.

248 The capability to independently tune both the size of the final  
249 fiber and its internal microfilaments provides the opportunity to  
250 implement current extrusion-based bioprinters while improving reso-  
251 lution down to cell-size scales. This multiscale biofabrication strategy  
252 specifically offers the formation of fibrous tissues with any target size  
253 while maintaining the capacity of the scaffold to direct cellular organi-  
254 zation. The multicompartamental microstructure further provides the  
255 opportunity to harness the advantages of different biomaterials.

## 256 B. Directing cellular organization with 257 multicompartamental hydrogel fibers

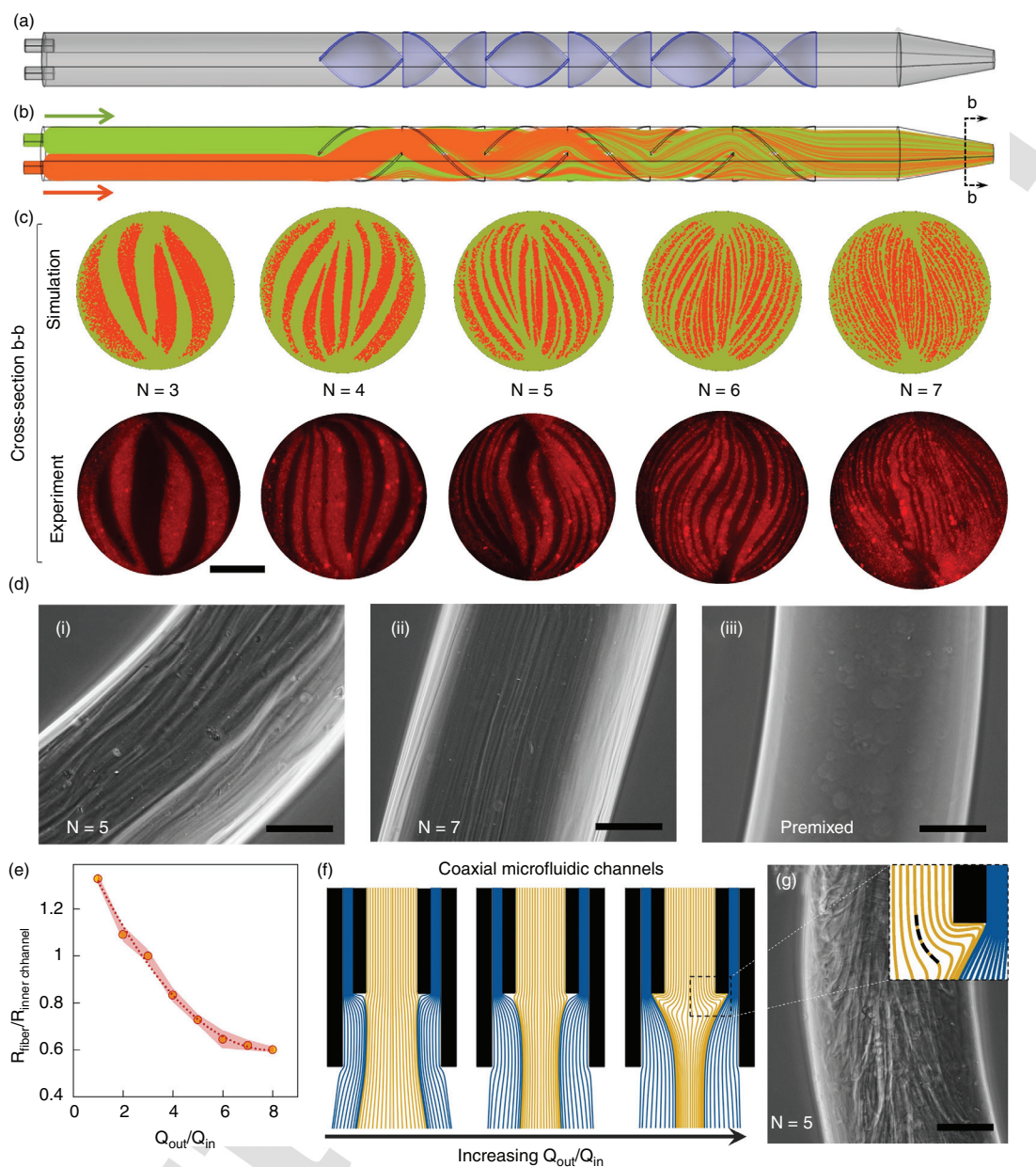
258 The multicompartamental fiber biofabrication strategy enabled  
259 directing cellular organization. Cells were encapsulated in GelMA pre-  
260 cursor, and MCHFs were fabricated as previously described. Figure 3  
261 compares the behavior of myoblasts cultured within the MCHFs with  
262 those cultured in fibers fabricated with premixed bioink. Despite the  
263 large ( $>1$  mm) diameter of the fibers compared with the cell size, a  
264 highly aligned cellular organization was observed in MCHFs 24 h  
265 postfabrication [Fig. 3(a)], while the cells encapsulated in premixed  
266 fibers remained almost spherical [Fig. 3(b)]. The cellular alignment  
267 within the multicompartamental hydrogel fibers can be explained by (i)  
268 differential favorability of the cells for spreading in GelMA microfila-  
269 ments over the alginate sections, (ii) fibrous internal microstructure  
270 acting as topological cues for directing cellular alignment, and (iii)  
271 mechanical stimulation of the cells due to differential mapping of scaf-  
272 fold stiffness in GelMA and alginate sections.

273 Since alginate does not have bioactive sequences, it acts as a cell-  
274 repellent compartment in the fiber structure, and therefore induces  
275 cell spreading inside internal GelMA microfilaments. Furthermore,  
276 the presence of 3D microtopographies of comparable size to the cell  
277 dimensions can direct cellular alignment along the microcompartment  
278 interfaces. As described previously, for a fiber with a diameter of  
279  $\sim 1$  mm, a static mixer with five to six Kenics elements forms internal  
280 GelMA microfilaments with an average size of  $15-30 \mu\text{m}$ . Our data  
281 suggest that a higher level of mixing leads to formation of fibers with-  
282 out distinct regions due to miscibility of aqueous GelMA and alginate  
283 precursors. Upon exposure to  $\text{Ca}^{2+}$  ions, alginate immediately cross-  
284 links, which is accompanied by structure shrinkage,<sup>42</sup> squeezing out  
285 the liquid GelMA from the construct before photocrosslinking (Fig.  
286 S3). A decreased level of mixing, which consequently reduces the  
287 entrapment of the GelMA striations, therefore causes leaching of large  
288 portions of GelMA, leaving behind only non-cell-permissive alginate.

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**FIG. 2.** Characterization of multicompartmental hydrogel fibers. (a) Representative design of Kenics static mixer with helical elements used for flow characterization via finite element simulations. (b) The working principle of the Kenics static mixer is demonstrated using simulation results. Two streams of hydrogel precursors were introduced at the inlets of the static mixer and then consecutively divided into substreams by Kenics elements followed by their blending as a result of helical profile of the elements. (c) A cross section of the multicompartmental stream (top row, simulation results) or fabricated hydrogel fiber (bottom row, experimental results) demonstrating the effect of number of elements on the number and size of internal microstructure.  $N$  stands for the number of consecutive elements in the mixer. Scale bar is  $500\ \mu\text{m}$ . (d) Phase contrast images of multicompartmental alginate/GelMA fibers demonstrating the fiber's internal microfilaments. Increasing the number of mixing elements decreased the size of the microfilaments. Subpanels (i) and (ii) correspond to the fibers fabricated using the Kenics static mixer with five and seven elements, respectively, while subpanel (iii) shows the fabricated fiber with a premixed bioink prepared through vortex mixing and heating at  $80\ ^\circ\text{C}$ . Scale bars are  $200\ \mu\text{m}$ . (e) The control over the fiber diameter using the coaxial microfluidic device. While the diameter of the fiber can be manipulated by changing the diameter of the internal channel in the coaxial device, it can also be tuned finely by adjusting the inner and outer channel flow rates ( $Q_{in}$  and  $Q_{out}$ , respectively).  $R_{fiber}$  and  $R_{inner\ channel}$  indicate the radius of the fabricated hydrogel fiber and the radius of the inner channel in the coaxial microfluidic device, respectively.  $n = 3$  for each measurement point. (f) The simulation results demonstrating the effect of  $Q_{out}/Q_{in}$  ratio on the diameter of the fabricated fiber. Blue streamlines show the flow of  $\text{CaCl}_2$ , and yellow streamlines represent the hydrogel mixture flow ( $Q_{out}/Q_{in} = 1, 3, \text{ and } 8$ , respectively, from left to right). (g) The effect of flow rates on organization of internal microfilaments. Increasing the  $Q_{out}/Q_{in}$  ratio deforms the streamlines of the hydrogel mixture and therefore changes the orientation of the internal microfilaments. Scale bar is  $200\ \mu\text{m}$ .

289 The difference in mechanical properties of alginate and GelMA  
 290 hydrogels can further induce cellular alignment as a result of mechani-  
 291 cal stimulation. Figure S4 demonstrates the significant difference  
 292 between mechanical properties of the alginate and GelMA hydrogels  
 293 used in this study. It has been shown that the presence of stiff geomet-  
 294 rical constraints (anchoring sites), which can restrict the movement of  
 295 cell-containing hydrogels, induce cellular alignment and maturation,  
 296 specifically in contractile tissues.<sup>43</sup> The cellular alignment in these sys-  
 297 tems arises from mechanical stimulation generated by a cytoskeleton-  
 298 mediated internal tension along the lines passing between the hydrogel  
 299 anchoring sites.<sup>15,44</sup> Many studies have reported the application of stiff  
 300 geometrical constraints for anchoring the cell-laden hydrogel and  
 301 therefore inducing cellular alignment.<sup>27,45</sup> Specifically, it has been  
 302 demonstrated that an alignment in the geometry of stiff anchoring  
 303 sites can align cells more effectively.<sup>43,44</sup> In our system, aligned alginate  
 304 microfilaments with significantly higher elastic modulus compared to  
 305 GelMA can act as anchoring sites, constraining the cell-laden GelMA  
 306 hydrogel, and therefore induce alignment. The application of alginate  
 307 as a stiff hydrogel within soft hydrogel networks has been previously  
 308 reported for controlling cellular shape and spreading.<sup>46</sup>

309 A quantitative evaluation of cell orientation in the multicompart-  
 310 mental hydrogel fibers demonstrated an almost uniaxial organization of  
 311 both cytoskeleton and nuclei along the fiber axis [Fig. 3(c)]. The align-  
 312 ment of the nuclei is of specific importance due to the crucial role of  
 313 nuclei morphology in cellular behavior, affecting their metabolic activity,  
 314 protein expression, and differentiation.<sup>3</sup> We further demonstrated that  
 315 the multicompartmental hydrogel fibers support cellular proliferation, in  
 316 contrast to the fibers fabricated from the premixed bioink [Fig. 3(d)].  
 317 The presence of distinct GelMA regions in the engineered construct  
 318 ensures cell spreading and proliferation. However, in the premixed struc-  
 319 ture, the presence of alginate does not allow scaffold degradation and  
 320 therefore does not offer enough space for proper cell spreading and pro-  
 321 liferation. As a result, the activity of the cells, and therefore their rate of  
 322 proliferation, decreased over time. Due to the limited biocompatibility of  
 323 the hydrogel fibers fabricated with premix bioink, specifically in longer-  
 324 term studies, we excluded them from the future experiments.

325 We demonstrated the potential of the proposed biofabrication  
 326 strategy for directing alignment of the cells along the fiber axis, while  
 327 supporting cellular activity and function. Since cells follow the fiber  
 328 direction (Fig. S5), their orientation inside the scaffold can be easily  
 329 controlled by adjusting the orientation of the fiber during bioprinting  
 330 or assembly of the fibers through biotextile methods. We have also  
 331 demonstrated the ability to control cellular alignment inside the indi-  
 332 vidual fibers (Fig. 4). As mentioned in Sec. IIA and indicated in Fig.  
 333 2(g), manipulation of flow rates in the microfluidic coaxial device pro-  
 334 vides the opportunity to change the orientation of internal hydrogel  
 335 microfilaments. This fact was exploited here to control the internal  
 336 organization of the cells. Because the encapsulated cells spread along  
 337 the internal microfilaments, the cellular alignment can be finely tuned  
 338 by controlling the flow rates. As shown in Fig. 4(a), increasing the ratio  
 339 of  $Q_{out}/Q_{in}$  can deviate the direction of cellular orientation from the  
 340 fiber axis toward a radial alignment perpendicular to the fiber axis.  
 341 While a static mixer with both five and six Kenics elements could  
 342 effectively generate MCHFs with controlled cellular organization, five  
 343 Kenics elements were used here to generate larger features and better  
 344 detect and characterize the cellular directionality. The quantitative  
 345 evaluation of F-actin direction indicates a unidirectional orientation in

the angled arrangement [Fig. 4(b)]. The adjustment of cellular orienta- 346  
 tion with flow rates enables continuous real-time control over the cel- 347  
 lular organization within the final scaffold. 348

### C. Cell differentiation in multicompartmental hydrogel fibers: Toward muscle tissue engineering 349 350

351 Fiber-based biofabrication approaches can be employed in pro- 352  
 duction of biomimetic scaffolds for engineering anisotropic tissues 353  
 such as muscle. Mimicking fibrillar structure of such tissues in bioen- 354  
 gineered scaffolds can regulate encapsulated cells' behavior toward 355  
 enhanced myogenesis.<sup>47–49</sup> Here, as a proof of concept, we have dem- 356  
 onstrated the ability of the proposed strategy for supporting myoblast 357  
 maturation (Fig. 5). The fibers were fabricated using the previously 358  
 described strategy, with a static mixer having six Kenics elements. A 359  
 $Q_{out}/Q_{in} = 1$  ratio was applied in the coaxial microfluidic system to 360  
 ensure the alignment of the microfilaments and therefore the encapsu- 361  
 lated cells along the fiber axis. Following fiber fabrication and their 362  
 subsequent culture for 24 h to allow cellular alignment, the maturation 363  
 of the myoblast was investigated by evaluating the morphology and 364  
 gene expression of the cells over time. As indicated in Fig. 5(a), the 365  
 aligned myoblasts rapidly proliferated, fused, and formed multinucle- 366  
 ated myotubes. On day 7 postencapsulation, the hydrogel fiber was 367  
 completely occupied by highly oriented densely packed myotubes, 368  
 forming a fascicle-like structure (Fig. S6).

369 To confirm the results obtained from the morphology analysis, 370  
 we further evaluated the expression of myogenic markers from the 371  
 myoblast-laden multicompartmental hydrogel fibers. The transcrip- 372  
 tional level of early and late myogenic markers was examined over 373  
 time using reverse-transcription quantitative polymerase chain reac- 374  
 tion (RT-qPCR). In muscle tissue formation, myogenic regulatory fac- 375  
 tors (MRFs), including myogenic differentiation (MyoD) and MRF4, 376  
 govern the differentiation of cells toward myofibers.<sup>17,50</sup> Figure 5(b) 377  
 schematically illustrates the myogenic progression of encapsulated 378  
 myoblast cells. At the initial differentiation step, aligned myoblasts 379  
 form myocytes and fuse with each other. These cells then experience 380  
 secondary fusion, creating myotubes, which can further form muscle 381  
 fibers. Finally, these myofibers mature to form fascicle-like constructs. 382  
 In this process, MyoD induces the expression of myogenin, which is 383  
 necessary for myocyte formation and fusion. In addition, MRF4 plays 384  
 a dual role, active both in proliferation of undifferentiated myoblasts 385  
 and as a differentiation gene in cells undergoing maturation. Both 386  
 myogenin and MRF4 have also been reported to contribute to terminal 387  
 differentiation.<sup>51,52</sup> Finally, in the matured muscle, sarcomere contrac- 388  
 tile proteins, such as myosin heavy chain 1 (Myh1), are highly 389  
 expressed, while MRF4 transcript levels exceed the expression of other 390  
 MRFs.<sup>17,50</sup> Here, the expression of MyoD in the cell-laden multicom- 391  
 partmental fibers peaked in days 5–7, indicating the differentiation of 392  
 myoblasts, while the MRF4 level showed a sharp increase on day 7, 393  
 demonstrating the maturation of the differentiated cells. High levels of 394  
 myosin heavy chain expression on day 11 further confirm the maturation 395  
 of cells and formation of fascicle-like structure.

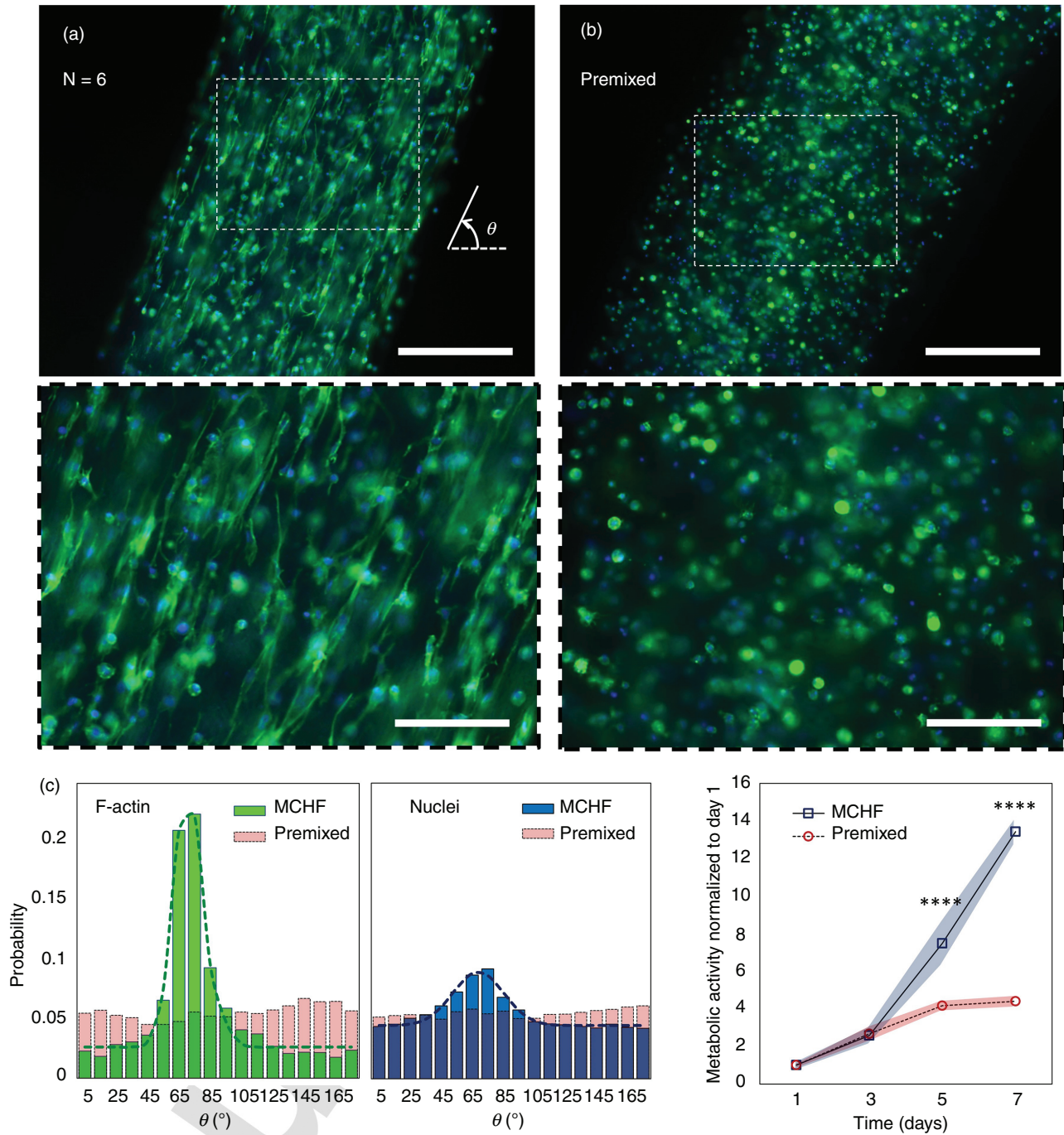
### D. Assembly of multicompartmental hydrogel fibers for fabrication of higher-scale constructs 396 397

398 One of the most important advantages of the proposed hydrogel 399  
 fiber formation is compatibility with existing fiber-based biofabrication

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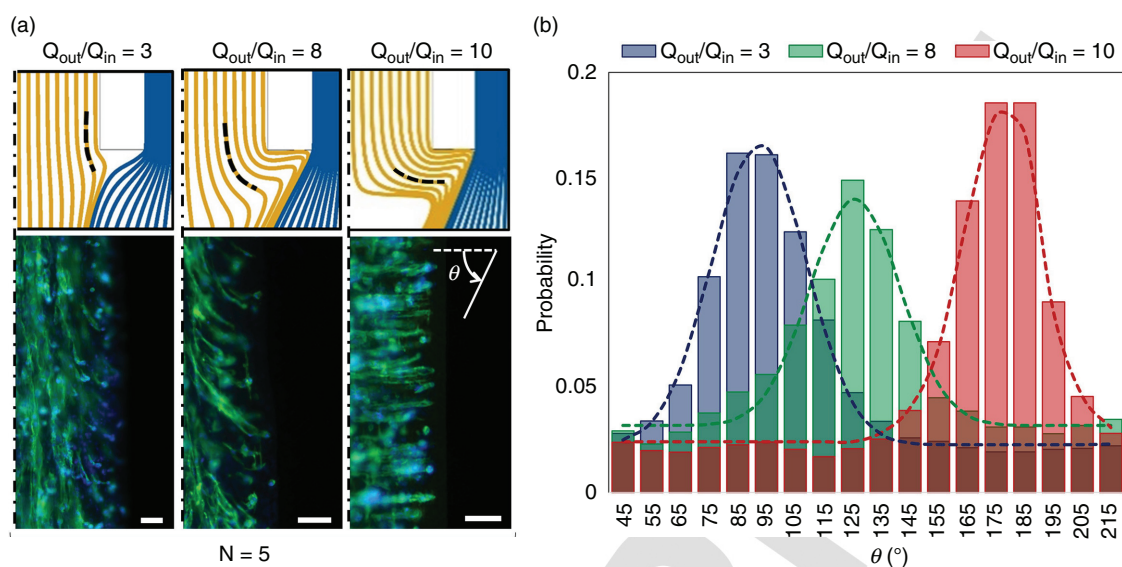
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**FIG. 3.** Cellular organization and metabolic activity in multicompartmental hydrogel fibers. (a) F-actin/DAPI staining demonstrating the alignment of myoblasts along the fiber axis 24 h postencapsulation. A static mixer with six Kenics elements was implemented for fabrication of multicompartmental alginate/GelMA fibers. The bottom image is a magnified representation of the zone indicated by dashed rectangle in the top image. (b) In contrast to the cells cultured in multicompartmental fibers, those cultured in premixed hybrid hydrogel fibers did not demonstrate spreading or alignment. The bottom image is a magnified representation of the zone indicated by the dashed rectangle in the top image. (c) Quantitative evaluation of F-actin cytoskeleton (left) and nuclei (right) directionality within MCHF compared with hydrogel fibers fabricated from premixed bioink. Although the size of the fibers was large compared with the cells' dimension ( $\sim 50$  times), a highly aligned unidirectional organization was observed both in the cytoskeleton and nuclei of the cells cultured in the MCHFs [ $\theta$  is shown in (a)]. (d) Enhanced metabolic activity of the cells cultured in MCHFs compared with the cells cultured in premixed fibers.  $n = 4$  for each time point. Scale bars are  $500 \mu\text{m}$  for the top row and  $200 \mu\text{m}$  for the bottom magnified images. \*\*\*\* $P < 0.0001$ .





**FIG. 4.** Real-time control of cellular organization within the multicompartmental fibers. (a) The effect of  $Q_{out}/Q_{in}$  ratio on cellular alignment. Increasing the ratio deviates the orientation of the cells in the fibers by deforming the hydrogel flow striations and, therefore, internal microfilament direction. The upper panels show the results of fluid dynamics simulations at the outlet of the microfluidic coaxial channels ( $Q_{out}/Q_{in} = 3, 8$ , and  $10$ , respectively, from left to right), while the lower panels show the corresponding cellular arrangement demonstrated using F-actin/DAPI staining. Dashed-dotted lines indicate center lines. Scale bars are  $500 \mu\text{m}$ . (b) Distribution of F-actin orientation at different ratios of flow rates, corresponding to the images shown in (a). A static mixer with five Kenics elements was used for formation of internal microfilaments.

400 methods for constructing higher-scale structures with physiologically  
 401 relevant dimensions (Fig. 6). Using an extrusion bioprinting device  
 402 [Fig. S1(b)], fibers were deposited to form a multicompartmental two-  
 403 layer mesh [Fig. 6(a), (i)] or unidirectional fibrous structures suitable  
 404 for mimicking anisotropic tissues [Fig. 6(a), (ii)]. A microscopic pic-  
 405 ture of the printed structure demonstrates that upon printing, the  
 406 internal microfilaments formed by the static mixer were preserved  
 407 [Fig. 6(a), (iii)]. The fibers can also be fabricated by wet spinning [Fig.  
 408 S1(c)] and assembled using various biotextile approaches [Fig. 6(b)].  
 409 The multicompartmental fibers were mechanically strong enough to  
 410 allow easy handling. The mechanical properties of fabricated fibers  
 411 with different concentrations of alginate and GelMA are shown in Fig.  
 412 S7. Since the proposed fiber fabrication strategy enables production of  
 413 relatively large fibers, while preserving the required resolution, the  
 414 handling challenges would be further reduced. In addition, the large  
 415 size of the fibers offers minimal assembly steps for production of  
 416 tissue-scale constructs. Figure 6(c) shows cell-laden assembled con-  
 417 structs fabricated through biotextile processes. The capability for  
 418 manipulation of the structure of assembled constructs by adjusting the  
 419 composition, microstructure, and cellular orientation of individual  
 420 fibers offers a high level of controllability in the biofabrication strategy.

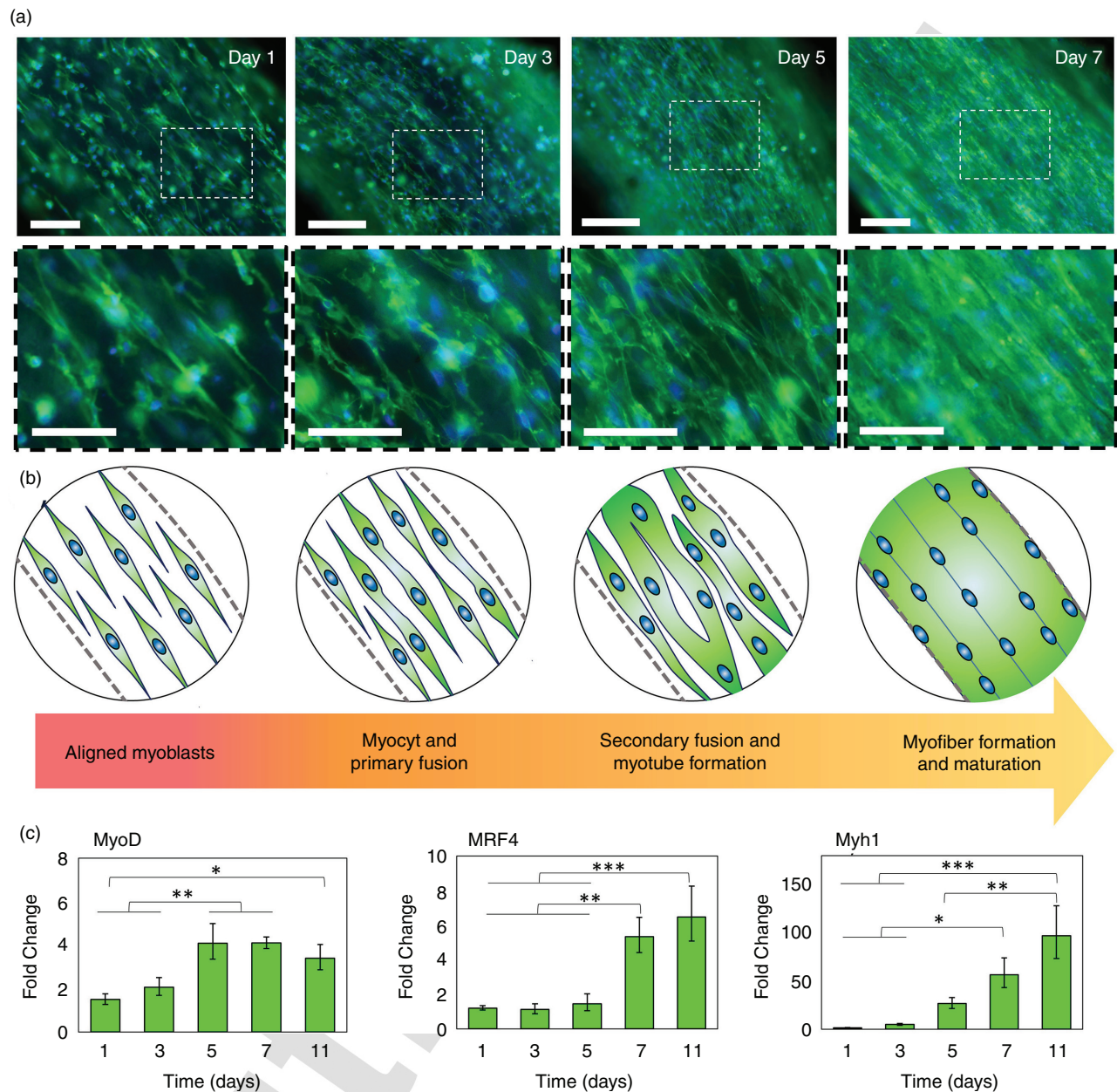
421 **III. DISCUSSION**

422 Controlling cellular organization in biofabrication strategies is  
 423 one of the most important, but challenging, requirements in engineer-  
 424 ing of highly organized tissues. This includes biomimetic spatial distri-  
 425 bution of the cells as well as specific cellular alignment within the  
 426 scaffolds. While the spatial distribution of the cells in the scaffolds can  
 427 be controlled by various top-down or bottom-up biofabrication  
 428 approaches, controlling the alignment of the cells during biofabrica-  
 429 tion is still an unmet need. The precise mimicking of cellular

organization in biofabrication has the potential not only to regulate  
 encapsulated cells' behavior toward formation of the target tissue but  
 also to promote the functionality of the final matured tissue. For  
 example, the proper alignment of cells within a muscle enhances the  
 force generation capacity of the tissue.<sup>53</sup> To form such cellular organi-  
 zation, a biofabrication strategy enabling high-resolution control over  
 the microstructure and patterned biomaterials is required. The resolu-  
 tion in the order of cell dimensions can ensure a proper regulation of  
 cellular alignment within the scaffold. To address this demand, a  
 methodology was designed based on two key elements:

1. A robust biofabrication strategy that
  - (i) can form scaffolds with controlled microstructure with  
feature size in the order of the cell dimension;
  - (ii) is compatible with bioprinting and biotextile assembly  
methods; and
  - (iii) is simple, low cost, and high throughput.
2. A suitable bioink that
  - (i) supports cell functionality by providing binding sites and  
biodegradable sequences;
  - (ii) forms stiff microtopographies to direct cellular alignment;
  - (iii) enables rapid cross-linking for compatibility with bio-  
printing and fiber spinning approaches; and
  - (iv) is mechanically strong enough to form a scaffold with  
high shape fidelity.

The biofabrication requirements were addressed by development  
 of a method having precise control over the flow of different hydrogel  
 precursors in a microfluidic nozzle. A Kenics static mixer with an opti-  
 mized number of helical elements was used to divide streams of differ-  
 ent hydrogel precursors and create aligned striations of hydrogels with

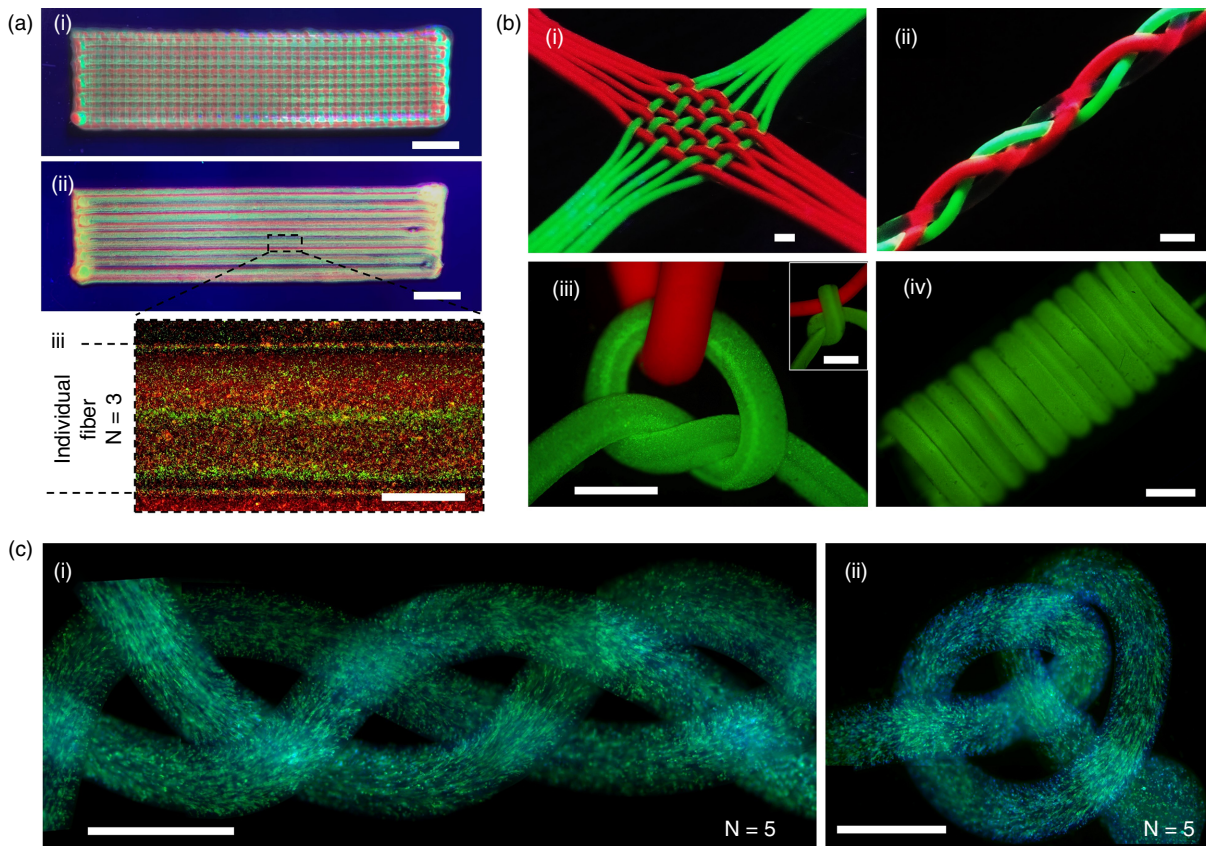


**FIG. 5.** Application of multicompartmental hydrogel fibers as a promising scaffold for muscle tissue engineering. (a) Morphology analysis of encapsulated myoblasts over a week using F-actin/DAPI staining. As illustrated, highly aligned cells rapidly proliferated, fused with each other, and differentiated toward muscle fiber formation. The bottom row represents the magnified images of the zones indicated in top row by dashed rectangles. Scale bars are  $200\ \mu\text{m}$  for the top row and  $100\ \mu\text{m}$  for the bottom row. (b) Schematic representation of myoblast myogenesis toward muscle fascicle formation. (c) Myogenic progression of the cells in hydrogel fibers using gene expression analysis with RT-qPCR. The expression of early (MyoD) and late (MRF4 and Myh1) myogenic markers was evaluated over 11 days. Fold change is calculated by normalizing the results to GAPDH as internal reference and day 0 results.  $n=3$  for each time point.  $*P < 0.05$ ,  $**P < 0.01$ ,  $***P < 0.001$ .

459 desired dimensions, comparable to the cell size. Using computational  
 460 fluid dynamics simulations, we demonstrated that the resolution in  
 461 this system is not shear or pressure dependent and is improved  
 462 through the consecutive subdivision of streams without changing the  
 463 nozzle diameter. This is an important advantage in fluidic systems,

specifically microfluidic devices applied in biofabrication of cell-laden 464  
 constructs. Conventionally, the resolution in extrusion bioprinting is 465  
 increased with the nozzle diameter. A fine nozzle diameter increases 466  
 the shear stress applied to the encapsulated cells and significantly 467  
 decreases their viability.<sup>54</sup> Additionally, the high pressure drop in fine 468





**FIG. 6.** Application of multicompartmental hydrogel fibers for biofabrication of higher-scale constructs. (a) Bioprinting of multilayered mesh (i) and unidirectional structures (ii). The microscopic picture (iii) confirms preservation of the internal microfilaments generated by a static mixer upon printing. Scale bars are 5 mm for (i) and (ii) and 500  $\mu\text{m}$  for (iii). Three Kenics elements were used for better visibility of different compartments along the fibers. (b) Various biotextile techniques, including weaving (i), braiding (ii), knotting (iii), and coil formation (iv), for biomimetic assembly of multicompartmental hydrogel fibers. The capability for manipulation of the structure of assembled constructs by controlling individual fiber composition is indicated by encapsulation of two different fluorescent particles in the fibers. Scale bars are 2 mm. (c) Cell-laden constructs fabricated through biotextile assembly of multicompartmental hydrogels. F-actin/DAPI assay was used for staining. Scale bars are 2 mm.

AQ7 469 nozzles, due to energy dissipation by channel wall-mediated hydrodynamic 470 resistance against the fluid flow, necessitates higher extrusion 471 pressure. A higher extrusion pressure can affect the cellular viability 472 and requires the application of pumps with higher power as well as 473 better channel sealing.<sup>54</sup> Finally, a fine nozzle decreases the throughput 474 of the bioprinting, which is of substantial importance in food biomani- 475 facturing.<sup>55</sup> The application of the static mixer in this study resolves 476 these important challenges. Subsequently, a coaxial microfluidic device 477 was implemented to extrude and form hydrogel fibers from the mixture 478 of the hydrogel precursor, controlling the diameter of the fiber 479 and the orientation of internal microfilaments.

480 Alginate and GelMA were selected to form the components of the 481 bioink in the proposed biofabrication technique. The bioink was 482 designed based on the synergistic interplay of these two materials in 483 which each hydrogel plays crucial roles for addressing the require- 484 ments of a suitable bioink. Using the biofabrication method, fibers 485 with internal microstructure consisting of consecutive microfilaments 486 of GelMA and alginate were formed. Within the microstructure, the 487 GelMA filaments provided a cell-permissive environment, while the

488 stiffer, non-cell-permissive alginate sections provided topological and 489 mechanical cues for cell alignment. By controlling the alignment of 490 microfilaments within the hydrogel fiber through manipulation of 491 flow rates in coaxial microchannels, we proposed a real-time control 492 mechanism over the direction of cellular orientation within the indi- 493 vidual fibers. This feature enables continuous bioprinting of cell-laden 494 constructs with *in situ*-controlled cellular organization.

495 We further demonstrated that this biofabrication strategy prop- 496 erly supports cellular activity within the scaffold, in contrast to the 497 hybrid scaffolds fabricated with homogeneously mixed alginate/ 498 GelMA hybrid bioink. This is an important outcome since several 499 efforts have been made to harness the printability of the alginate and 500 cell permissibility of the GelMA by application of their hybrid hydro- 501 gels, although the internal cell spreading and alignment were lim- 502 ited.<sup>29,36,37</sup> This issue could not be resolved even by introduction of 503 microfilaments inside fiber using a similar static mixer used in this 504 study.<sup>41</sup> This is due to the presence of alginate within the structure, 505 which prevents degradation, and therefore spreading and proliferation, 506 of the encapsulated cells. Here, we demonstrated that



507 microcompartmentalization in the structure can resolve this problem.  
508 Cells can spread and proliferate in the GelMA sections while alginate  
509 provides a matrix that allows a printable scaffold with high fidelity.

510 As a proof of concept, we demonstrated that the multicompart-  
511 mental hydrogel fibers support cellular maturation toward muscle tis-  
512 sue engineering. The biofabricated hydrogel fibers with internal  
513 microfilaments along the fiber axis provide the opportunity for  
514 improved mimicking of native muscular tissues and direct myoblast  
515 alignment. Staining and gene expression analysis confirmed the high  
516 potential of the multicompartmental hydrogel fiber for myogenesis.  
517 Fascicle-like constructs with densely packed, highly aligned cellular  
518 organization were formed, expressing genes associated with myofiber  
519 maturation.

520 The proposed biofabrication strategy is simple and robust. This  
521 system can be easily integrated with any extrusion bioprinting or fiber  
522 spinning device to fabricate multicompartmental scaffolds capable of  
523 controlling cellular alignment. As a result, we believe that this strategy  
524 can provide many opportunities for engineering of highly organized  
525 cellular scaffolds.

## 526 IV. MATERIALS AND METHODS

### 527 A. Materials

528 Sodium alginate (medium viscosity),  $\text{CaCl}_2$ , type A gelatin from  
529 porcine skin, methacrylic anhydride (MA), and 4',6-diamidino-2-phen-  
530 ylindole (DAPI) were purchased from Sigma-Aldrich. Irgacure 2959  
531 (CIBA Chemicals) was used as photoinitiator (PI). Dulbecco's phos-  
532 phate buffer saline (DPBS, Gibco), Hank's balanced salt solution  
533 (HBSS, Gibco) without calcium and magnesium, Dulbecco's modified  
534 eagle medium (DMEM, Gibco), fetal bovine serum (FBS, Gibco),  
535 horse serum (Gibco), and penicillin/streptomycin (Gibco) were used  
536 for experiments with the cells. Alexa Fluor 488 Phalloidin (Life  
537 Technologies) was used for characterization of cells' morphology,  
538 while metabolic activity of the cells was examined using PrestoBlue  
539 cell viability assay (Invitrogen).

### 540 B. Hydrogel preparation

541 GelMA was prepared according to the well-established proto-  
542 col,<sup>56</sup> with some modification. Briefly, a 10% solution of gelatin (in  
543 DPBS) was prepared by stirring for 1 h at 50 °C. Subsequently, 50  $\mu\text{l}$   
544 MA per 1 g gelatin was added to the mixture slowly and stirred for 3 h  
545 at 50 °C and 250 rpm to perform the methacrylation. To stop the reac-  
546 tion, DPBS was added (5:1 ratio of DPBS:GelMA), and dialysis was  
547 performed at 40 °C for 5 days using 12–14-kDa molecular weight cut-  
548 off tubing (Thermo Fisher Scientific). Finally, the solution was filtered,  
549 frozen at –80 °C for 2 days, and lyophilized for 5 days. GelMA precur-  
550 sor was prepared by mixing 2% PI and 10% GelMA solutions in HBSS  
551 with a 1:5 volumetric ratio. The alginate precursor was prepared at a  
552 2% concentration in HBSS.

### 553 C. Biofabrication of multicompartmental hydrogel 554 fibers

555 The biofabrication was performed through either bioprinting or  
556 wet spinning of multicompartmental hydrogel. In both cases, a static  
557 mixer integrated with a coaxial microfluidic device was used as the  
558 nozzle [Fig. S1(a)]. The static mixer was prepared by fitting a specific  
559 number of 3D-printed Kenics helical elements (66:100:4 ratio of

diameter:length:thickness of each element) into a barrel with a conical  
560 outlet. The barrel was then sealed with a polydimethylsiloxane plug  
561 with two openings for hydrogel injection. The microfluidic device for  
562 coaxial flow was fabricated by assembling blunt needles with different  
563 gauge sizes (14G and 18G or 19G and 24G). The needles were  
564 trimmed to such a size that the tip of the inner needle was located at  
565  $\sim 1$  mm from the opening of the outer one. Finally, the microfluidic  
566 device was attached to the conical static mixer tip. For experiments  
567 with cells, the device was incubated in ethanol (70%) followed by  
568 washing with autoclaved distilled water three times.  
569

570 To accurately adjust the flow rates of hydrogel and  $\text{CaCl}_2$  solu-  
571 tions, the inlets were connected to syringes using Tygon tubing (Cole-  
572 Parmer), and the flows were controlled using syringe pumps (PHD  
573 2000; Harvard Apparatus). Unless otherwise stated, the flow rates of  
574 alginate, GelMA, and  $\text{CaCl}_2$  solutions were set to 1 $\times$ , 1 $\times$ , and 2 $\times$ , in  
575 which the  $\times$  for bioprinting and wet spinning experiments were set to  
576 10  $\mu\text{l}/\text{min}$  and 500  $\mu\text{l}/\text{min}$ , respectively. In bioprinting experiments,  
577 the setup was mounted on the printing head of the bioprinter  
578 (Allevi 3). While the flow rates were controlled using separate syringe  
579 pumps, the displacement of the nozzle was controlled by the bio-  
580 printer [Fig. S1(b)]. For wet spinning [Fig. S1(c)], the nozzle was  
581 placed into a  $\text{CaCl}_2$  bath at 10 °C while the solutions were extruded. A  
582 2% (w/v)  $\text{CaCl}_2$  solution was used for ionic gelation of alginate fol-  
583 lowed by 30-s UV cross-linking of the GelMA using a 365 nm/850  
584 mW source placed at a distance of 7 cm from the fibers.

### 585 D. Fluid flow characterization and hydrogel fiber 586 topography

587 Finite element simulations were conducted to evaluate the func-  
588 tion of the static mixer and flow-focusing device and to examine the  
589 mechanism of highly aligned fibrillar structure formation within the  
590 hydrogel fiber. The model was implemented in COMSOL  
591 Multiphysics Version 5 using "Laminar Flow" and "Particle Tracing  
592 for Fluid Flow" interfaces. First, a 3D model was designed with the  
593 dimensions matching the dimensions of the actual static mixer and  
594 coaxial microfluidic device. The "Laminar Flow" was then used to sim-  
595 ulate the flow of hydrogel and  $\text{CaCl}_2$  solutions in the channels through  
596 solving the Navier-Stokes equations. Different flow rates were applied  
597 to the hydrogel and  $\text{CaCl}_2$  inlets in different simulations, correspond-  
598 ing to the experimental flow rates mentioned in Sec. IV C, while the  
599 relative pressure was always set to zero at the outlet. All boundaries  
600 were considered to have a "nonslip" condition, and the model was dis-  
601 cretized with fine free tetrahedral elements. Finally, the model was  
602 solved using "Stationary Solver." To evaluate the pressure inside the  
603 channels, the pressure obtained through solving the Navier-Stokes  
604 equations (the relative pressure  $p = p_{\text{abs}} - p_{\text{ref}}$  in which  $p_{\text{abs}}$  is the  
605 absolute pressure and  $p_{\text{ref}}$  is the sea-level pressure) was used.  
606 Additionally, the shear stress was calculated postsimulation through  
607 multiplication of shear rate (spf.sr) by the fluid viscosity (spf.mu). The  
608 maximum pressure  $P_{\text{max}}$  and the maximum shear stress  $\tau_{\text{max}}$  were  
609 determined from the highest values in the simulation domains pro-  
610 vided by the software. The maximum pressure generally happens at  
611 the channel entrance since it depends on resistance against the flow,  
612 while the maximum shear stress usually happens at the fluid/wall  
613 interface, where the channel cross-section area is minimum, because it  
614 is proportional to the rate of velocity changes. To track the streams of  
615 the hydrogels in the static mixer and for the cross-section profile, the

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- 616 “Particle Tracing for Fluid Flow” interface was used to simulate the  
617 movement of  $10^4$  massless particles in the previously solved velocity  
618 field using “Time Dependent Solver.” For particle tracing, a “Freeze”  
619 boundary condition was set to the channels’ walls. To visualize the  
620 fiber cross section in the simulations, “Poincaré Map” was imple-  
621 mented, with different colors used for the particles injected from dif-  
622 ferent inlets.
- 623 Experimentally, fluorescent particles were used to evaluate the  
624 cross-sectional profiles of the fibers. After fabrication, fibers were  
625 embedded into 3% agarose gel and sliced using a surgical blade. To  
626 evaluate the formation of GelMA microfilaments in the alginate  
627 matrix, phase contrast microscopy was performed on a Zeiss Observer  
628 D1 microscope. The diameter of final fibers was measured using ZEN  
629 2 software.
- 630 E. Cell culture**
- 631 Murine myoblast cell line C2C12 (ATCC) was cultured in  
632 DMEM supplemented with 10% [volume/volume (v/v)] FBS and 1%  
633 (v/v) penicillin/streptomycin (culture medium). Cells were incubated  
634 at 37 °C in a humidified 5% CO<sub>2</sub> atmosphere and subcultured at  
635 80%–90% confluence. Cell passages 6–8 were utilized for experiments.
- 636 For the encapsulation of C2C12 myoblasts, cells were trypsinized  
637 and detached followed by resuspension in culture medium with the  
638 density of  $20 \times 10^6$  cells/ml. The solution was then added to GelMA  
639 precursor with the volumetric ratio of 1:20 and mixed. Subsequently,  
640 cell-laden multicompartmental hydrogel fibers were formed as previ-  
641 ously described. After fabrication, the fibers were incubated in the cul-  
642 ture medium for future analysis. For evaluating maturation of the  
643 myoblasts in the scaffolds, culture medium was replaced with differen-  
644 tiation medium 2 days after biofabrication. The differentiation  
645 medium, which was prepared using DMEM supplemented with 2%  
646 (v/v) horse serum and 1% (v/v) penicillin/streptomycin, was replaced  
647 every 48 h.
- 648 F. Cellular morphology characterization**
- 649 F-actin/DAPI staining was employed for characterization of cells’  
650 morphology. The staining was conducted at room temperature, and  
651 HBSS was used for washing steps and solution preparation. Samples  
652 were fixed using 4% paraformaldehyde (Electron Microscopy  
653 Sciences) for 30 min, washed three times, and stained using phalloidin  
654 and DAPI as described in the manufacturer’s manual, with small mod-  
655 ifications. Briefly, cells were permeabilized using 0.2% (v/v) Triton X-  
656 100 (Sigma) for 10 min, washed three times, and followed by blocking  
657 with 1% (w/v) bovine serum albumin (Sigma). The samples were then  
658 incubated for 40 min in phalloidin (1.65  $\mu$ M), protected from the light,  
659 and subsequently washed three times. Nuclei of the cells were then  
660 stained using DAPI solution (5  $\mu$ g/ml) for 15 min, and finally, the  
661 samples were washed three times. Fluorescence microscopy was per-  
662 formed on the Zeiss Observer D1 microscope employing an X-Cite  
663 120Q fluorescence source. Subsequently, quantitative analysis of the  
664 cellular orientation was performed using Directionality or  
665 Orientation] plugins of FIJI open-source software.<sup>57</sup>
- 666 G. Determination of metabolic activity**
- 667 Metabolic activity of the encapsulated myoblasts within the  
668 hydrogel fiber constructs was measured using a PrestoBlue viability
- assay. For this purpose, the fabricated hydrogel fibers were cut into  
smaller segments ( $\sim$ 1 cm) and incubated with 10% PrestoBlue solu-  
tion (v/v in culture medium) at 37 °C. After 1 h, the solution was col-  
lected in a 96-well plate, and its fluorescent intensity (550 ex/600 em)  
was measured using a plate reader (Synergy 2; BioTek). The evaluation  
was performed 1, 3, 5, and 7 days after fiber fabrication. The back-  
ground intensity (corresponding to wells with 10% PrestoBlue solu-  
tion, excluding cell-laden fibers) was subtracted, and the results were  
normalized with respect to the values of day 1.
- H. Reverse-transcription quantitative polymerase chain reaction**
- Expression levels of three myoblast differentiation genes (MyoD, MRF4, and Myh1) were evaluated using RT-qPCR after 0, 1, 3, 5, 7, and 11 days of fiber fabrication. Total RNA was extracted using RNeasy Plus Mini Kit (QIAGEN), and 1  $\mu$ g of extracted RNA was reverse-transcribed using QuantiTect Reverse Transcription Kit (QIAGEN) according to the manufacturer’s protocols. Real-time PCR was performed on a Rotor-Gene Q (QIAGEN) using 2  $\mu$ l cDNA template, 2  $\mu$ l primer set, and 16  $\mu$ l SYBR Green Master Mix (Fermentas). Thermal cycle conditions were 10 min denaturation at 95 °C followed by 45 cycles of 10 s at 95 °C, 30 s at 60 °C, and 30 s at 72 °C. The results were normalized to that of GAPDH as reference housekeeping gene and then to the results of day 0 using  $2^{-\Delta\Delta C_t}$  method. The primer sequences used for amplification are listed in Table S1.
- I. Statistical analysis**
- All experiments were performed at least in triplicate, and the results were presented as average  $\pm$  standard deviation. Comparison between the groups was performed through one- or two-way analysis of variance, and results were presented as \* $P < 0.05$ , \*\* $P < 0.01$ , \*\*\* $P < 0.001$ , and \*\*\*\* $P < 0.0001$  in which  $P$  is the adjusted  $P$  value.
- AUTHORS’ CONTRIBUTIONS**
- M.S. and A.T. conceived and designed the research. M.S. and F.A. performed the experiments. M.S., K.M.-A., and A.T. analyzed the results. M.S., K.M.-A., M.M.A., G.T.-d.S., and A.T. participated in writing the manuscript. All authors contributed to revising and editing the manuscript.
- SUPPLEMENTARY MATERIAL**
- See the [supplementary material](#) for additional information on the applied devices, further characterization of the bioprinted MCHFs, and primer design for gene expression analysis.
- ACKNOWLEDGMENTS**
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- DATA AVAILABILITY**
- The data that support the findings of this study are available within the article and its [supplementary material](#). Additional data that

720 support the findings of this study are available from the corresponding  
721 author upon reasonable request.

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